METHOD OF STARTING BRUSHLESS DC MOTOR ON THE BASIS OF INDUCED VOLTAGE IN ARMATURE COIL FOR DETECTION OF POSITION OF ROTOR

Background of the Invention

1. Field of the Invention

The present invention is related to a method of starting a brushless DC motor. The present invention is especially related to a method of starting a brushless DC motor in which a position of the rotor is detected on the basis of an induced voltage in the armature coil.

2. Description of the Related Art

A brushless DC motor that does not contain a hall element for detecting a position of the rotor is widely used. The brushless DC motor detects a voltage induced in an armature coil by a rotation of the rotor, and determines the position of the rotor. In response to the position of the rotor, a drive current is supplied to the armature coil to rotate the rotor.

To start the brushless DC motor, various methods are proposed which does not rely on the induced voltage, since no voltage is induced in the armature coil while the rotor is in a stationary state.

A first conventional method of starting a brushless DC motor is disclosed in Japanese Laid Open Patent Application (JP-A-Heisei, 9-233885). With reference to Fig. 1A, an electric current

5 firstly is supplied to flow from a U-phase coil 101 to a V-phase coil 102 for a short time, and thereby a rotor 103 is rotated in a direction indicated by an arrow 104. While the electric current is supplied, the rotor 103 is locked at a

10 position shown in Fig. 1B. In succession, a drive current is supplied to flow from a W-phase coil 105 to the V-phase coil 102, and the rotor 103 begins to rotate in a counterclockwise direction. Then, the drive current is sequentially switched

15 to the phase coils 101, 102, and 105 so that the rotor 103 is accelerated. After the increase in the rotation speed of the rotor 103, the position of the rotor 103 is detected from the electromotive voltage induced in the phase coils

20 101, 102 and 105 and the drive current is switched on the basis of the detected position.

In the first conventional method of starting a brushless DC motor, however, it takes a long time for the rotor 103 to be locked at a

25 certain position. A considerable time is needed for the rotor 103 to be fixed because of inertia of the rotor 103. The time required to start a

brushless DC motor is desired to be short.

A second conventional method of starting a brushless DC motor is disclosed in "Transistor Technique, Feb. 2000" pp.221 to 228. In addition, a conventional brushless DC motor system using the second conventional method of starting a brushless DC motor is disclosed in Japanese Laid Open Patent Application (JP-A-Heisei 8-308288). As shown in Fig .2, the conventional brushless DC motor system is provided with a DC brushless motor 111, a microcomputer 112, an output unit 113, a position detector 114 and a electrically programmable memory 115. A three-phase armature current is supplied in accordance with a drive pattern stored in the memory 115. The drive pattern has no relation to a position of a rotor of the motor 111. The microcomputer 112 controls the output unit 113 in accordance with the drive pattern stored in the memory 115.

However, the conventional brushless DC motor is large in circuit size, because the memory 115 requires a large circuit size.

Moreover, the second conventional method of starting the brushless DC motor requires a long time until the rotation of the rotor is achieved. Furthermore, the second conventional method of actuating a brushless DC motor can not obtain a

large actuation torque. These results from that an armature current is supplied to the armature coil in accordance with a certain drive pattern, irrespectively of the position of the rotor.

5   A third conventional method of starting a brushless DC motor is disclosed in the above-mentioned "Transistor Technique, Feb. 2000" pp.221 to 228. In the third conventional method, a position of a stationary rotor is detected from
10 an increase speed of an armature current when an armature voltage is applied to an armature coil.

          Figs. 3A, 3B and 3C show the third known method of starting a brushless DC motor. Suppose that a rotor 121 and an armature 122 of the
15 brushless DC motor are located at positions shown in Fig. 3A.

          At first, A three-phase drive voltage is applied to the armature 122 in accordance with a voltage pattern shown in Fig. 3B. The drive
20 voltage pattern is switched at a high speed so that the rotor 122 is not rotated.

          When the three-phase drive voltage is applied to the armature 121, the increase speed of the current flowing through the armature 121
25 depends on the position of the rotor 122. If a direction of a magnetic field generated by the armature 121 coincides with a direction of a

magnetic field generated by a magnet 122a placed
in the rotor 121, the current quickly increases.
With reference with Fig. 3B, let us suppose that
a U-phase drive voltage V_U is set at a power

5   supply potential V_{cc}, and a V-phase drive voltage
V_V is set at a ground potential, respectively at a
timing (1). In this case, a U-phase coil 121a
generates a magnetic flux in a direction
substantially coincident with a direction of a

10 magnetic flux generated by a magnet 122a opposite
to the U-phase coil 121a. In this case, a current
I_U flowing through the U-phase coil sharply
increases, as shown in Fig. 3C.

On the other hand, if the direction of the

15 magnetic field generated by the armature 122 does
not coincide with the direction of the magnetic
field generated by the magnet 122a placed in the
rotor 122, the increase speed of the current is
slow. As shown in Fig. 3B, at a timing (4), let

20 us suppose that the U-phase drive voltage V_U is
set at the ground potential, and the V-phase
drive voltage V_V is set at the power supply
potential V_{cc}, respectively. The U-phase coil
121a generates a magnetic flux in a direction

25 opposite to the direction of the magnetic flux
generated by the magnet 122a opposite to the U-
phase coil 121a. In this case, the current I_U

flowing through the U-phase coil is slow, as
shown in Fig. 3C.

In this way, the increase speed of the
armature current when the armature voltage is
5   applied to the armature implies the relative
position between the rotor and the armature. Thus,
the position of the stationary rotor is detected
from the increase speed. The motor is started on
the basis of the detected position of the rotor.

10   A circuit for detecting the increase speed
of the armature current is required in order to
embody the third known method of actuating a
brushless DC motor. Typically, such a circuit
requires a configuration of an analog circuit. If
15   the analog circuit is integrated into LSI, the
occupation area becomes wide. Thus, if the
circuit for detecting the increase speed of the
current is integrated into the LSI, the area
occupied by its circuit becomes wide. The size of
20   the circuit for starting the brushless DC motor
is desired to be small.

Also, a fourth conventional method of
starting a brushless DC motor is disclosed in
Japanese Laid Open Patent Application (Jp-A-
25   Heisei 6-237595). In the fourth conventional
method, a starting current supplied to the
armature coil has a waveform determined to

increase the starting torque and to avoid the failure of the start.

Summary of the Invention

5   Therefore, an object of the present invention is to reduce a time required to start a brushless DC motor.

Another object of the present invention is to reduce a size of a circuit required to start a
10   brushless DC motor.

Still another object of the present invention is to reduce an area occupied by an integrated circuit for starting a brushless DC motor.

15   In order to achieve an aspect of the present invention, a method of starting a brushless DC motor including an armature coil in a stator and field magnets in a rotor is composed of:

20   supplying a starting current for the armature coil while the rotor is in a stationary state;

measuring an induced voltage induced in the armature coil by rotation of the rotor wherein
25   the rotation is caused by the starting current; and

supplying a drive current for the armature

coil in response to the induced voltage.

The supplying of the drive current preferably includes:

determining a position of the rotor based on the induced voltage, and

deciding the drive current based on the position.

The measuring of the induced voltage may be executed after the supplying the starting current.

The measuring of the induced voltage may be executed during the supplying the starting current.

The supplying of the starting current preferably includes:

supplying another starting current for the armature coil, and

supplying the starting current when the rotor is not rotated by the another starting current. The starting current and the another starting current have different waveforms each other.

The method of starting the brushless DC motor is preferably further composed of:

detecting a direction of the rotation, and

stopping the rotor when the direction is not a desirable direction.

The supplying of the drive current

preferably includes:

continuously supplying a first drive current for the armature coil till a speed of the rotation becomes a predetermined speed, the first drive current being determined based on the induced voltage, and

supplying a second drive current for the armature coil after the continuously supplying the first drive current, a current flow duration of the second drive current being controlled based on the speed.

The supplying of the drive current preferably includes:

supplying a first drive current for the armature coil such that the rotor is rotated with a maximum torque, till a speed of the rotation becomes a predetermined speed; and

supplying a second drive current for the armature coil after the supplying the first drive current, a current flow duration of the second drive current being controlled based on the speed.

In order to achieve another aspect of the present invention, a brushless DC motor is composed of an armature including an armature coil, a rotor including a plurality of field magnets, a power supply unit, and a measuring unit. The power supply unit supplies a starting

current for the armature coil while the rotor is
in a stationary state. The measuring unit
measures an induced voltage induced in the
armature coil by rotation of the rotor that is
5   caused by the starting current. The power supply
unit supplies a drive current for the armature
coil in response to the induced voltage.

Brief Description of the Drawings

10   Fig. 1A is a view describing a conventional
method of starting a brushless DC motor;

Fig. 1B is a view describing the
conventional method of starting a brushless DC
motor;

15   Fig. 2 is a view showing a configuration of
a conventional brushless DC motor to which
another conventional starting method is applied;
and

Figs. 3A, 3B and 3C are views describing
20   still another conventional method of starting a
brushless DC motor.

Fig. 4 shows a configuration of a brushless
DC motor of an embodiment according to the
present invention;

25   Fig. 5 shows a method of starting a
brushless DC motor of the embodiment;

Fig. 6 shows starting patterns; and

Fig. 7 shows potentials of a U-phase line 9a, a V-phase line 9b and a W-phase line.

Description of the Preferred Embodiments

5   A brushless DC motor system according to the present invention and a method of starting the same will be described below with reference to the attached drawings.

As shown in Fig. 4, the brushless DC motor

10   system of the embodiment according to the present invention is provided with a brushless DC motor 1, an induced voltage detector 2 and a driver 3.

The brushless DC motor 1 contains an armature 4 and a rotor 5. The armature 4 has a U-

15   phase coil 4a, a V-phase coil 4b and a W-phase coil 4c. The U-phase coil 4a, the V-phase coil 4b and the W-phase coil 4c constitute a star connection, being connected at a neutral point 4d. A U-phase line 9a, a V-phase line 9b and a W-

20   phase line 9c are respectively connected to the U-phase coil 4a, the V-phase coil 4b and the W-phase coil 4c. A three-phase armature current are supplied through the U-phase line 9a, the V-phase line 9b and the W-phase line 9c to the U-phase

25   coil 4a, the V-phase coil 4b and the W-phase coil 4c, and the supplied three-phase armature current drives the rotor 5 to rotate.

The induced voltage detector 2 measures the electromotive voltages induced in the U-phase coil 4a, the V-phase coil 4b and the W-phase coil 4c by the rotation of the rotor 5. A potential of

5 the neutral point 4d is used as a standard potential for the measurement of the electromotive voltages. The induced voltage detector 2 sends a voltage measurement signal a to inform the driver 3 of the measured

10 electromotive voltages.

The driver 3 supplies the three-phase armature current to the armature 4 in response to the measured electromotive voltages. The driver 3 supplies the three-phase armature current through

15 the U-phase line 9a, the V-phase line 9b and the W-phase line 9 to the armature 4.

The driver 3 contains a drive operator 6, an output unit 7 and a start pattern generator 8.

The drive operator 6 calculates the

20 position of the rotor 5 on the basis of the measured electromotive voltages. The drive operator 6 determines a supply timing of the three-phase armature current in accordance with the calculated position of the rotor 5 and

25 generates a timing indication signal d to inform the output unit 7 of the supply timing.

The output unit 7 pulls the U-phase line 9a,

the V-phase line 9b and the W-phase line 9c up to

a power supply potential V_{cc}, or pulls them down

to a ground potential, or set them to a floating

state, at the timing indicated by the timing

5   indication signal d. That is, the output unit 7

supplies the three-phase armature current to the

armature 4 in response to the timing indication

signal d.

Here, before the brushless DC motor 1 is

10   started, no electromotive voltage is induced in

the U-phase coil 4a, the V-phase coil 4b and the

W-phase coil 4c, and the position of the rotor 5

can not be detected. To start the brushless DC

motor 1, the starting pattern generator 8 is

15   provided in the driver 3.

The starting pattern generator 8 determines

a starting current pattern of the starting

current supplied to the armature 4 when the

brushless DC motor 1 is started. The start

20   pattern generator 8 outputs a starting pattern

indication signal b indicative of the determined

starting current pattern to the drive operator 6.

When the brushless DC motor 1 is started, the

drive operator 6 determines a supply timing of

25   the starting current supplied to the armature 4

in accordance with the starting current pattern,

and generates a timing indication signal c. The

output unit 7 supplies the current to the armature 4 at the timing indicated by the timing indication signal c.

At this time, even if the starting current
5 is supplied in accordance with the starting current pattern, the brushless DC motor 1 fails to be started. In such cases, the drive operator 6 outputs a start pattern change indication signal d to the start pattern generator 8. The
10 start pattern generator 8 changes the starting current pattern in response to the starting current pattern change indication signal d.

The method of starting a brushless DC motor will be described in detail below with reference
15 to Fig. 5.

At first, the start pattern generator 8 determines a starting current pattern (Step S01). The starting current pattern is selected from among Patterns 1 to 6 shown in Fig. 6.

20 If Pattern 1 is selected, a starting current is supplied to flow from the V-phase coil 4b to the U-phase coil 4a. If Pattern 2 is selected, a starting current is supplied to flow from the V-phase coil 4b to the W-phase coil 4c.

25 Similarly, if Patterns 3 to 6 are selected, a starting current is supplied to flow from the U-phase coil 4a to the W-phase coil 4c, from the U-

phase coil 4a to the V-phase coil 4b, from the W-phase coil 4c to the V-phase coil 4b, and from the W-phase coil 4c to the U-phase coil 4a, respectively.

5   Armature voltages applied to the U-phase line 9a, the V-phase line 9b and the W-phase line 9c are determined on the basis of the selected starting current pattern. In Fig. 6, the "GND"s imply the setting at the ground level. The "VCC"s

10   imply the setting at the power supply potential V_{cc}. The "NC"s imply the setting at the floating state.

When the brushless DC motor is started, Pattern 1 is firstly selected as the starting

15   current pattern. The fact that Pattern 1 is selected as the starting current pattern is reported to the drive operator 6 by the starting pattern indication signal b. As described later, when the brushless DC motor 1 is not started by

20   the use of Pattern 1, another pattern among Patterns 2 to 6 is selected as the starting current pattern.

In succession, a starting current is applied to the armature 4 in accordance with the

25   determined starting current pattern (Step S02). At this time, the drive operator 6 outputs the timing indication signal c to the output unit 7

in response to the starting pattern indication signal b to instruct the output unit 7 to supply the starting current from the V-phase to the U-phase for T seconds. The period of T seconds is

5 selected such that it is positively slight within a range in which the rotor 5 can be rotated.

For the T seconds, the output unit 7 sets the U-phase line 9a at the ground level, and sets the V-phase line 9b at the power supply potential

10 V_{cc}, and sets the W-phase line 9c at the floating state to supply the starting current from the U-phase to the V-phase. In many cases, the starting current slightly rotates the rotor 5 by electromagnetic force.

15 In succession, the electromotive voltage induced by the rotation of the rotor 5 is measured (Step S03). At this time, the output unit 7 sets all of the U-phase line 9a, the V-phase line 9b and the W-phase 9c at the floating

20 state. The slight rotation of the rotor 5 induces the electromotive voltages in the U-phase coil 4a, the V-phase coil 4b and the W-phase coil 4c of the armature 4. The induced electromotive voltages are measured from the potentials of the

25 U-phase line 9a, the V-phase line 9b, the W-phase line 9c and the neutral point 4d of the armature 4, respectively. The measured electromotive

voltages are reported on the voltage measurement signal a to the drive operator 6.

The electromotive voltage may be measured while the starting current is applied to the

5   armature 4. As described above, at the time of the starting, the starting current flows from the U-phase to the V-phase, and the W-phase line 4b is set at the floating state. The electromotive voltage induced in the W-phase coil 4c can be

10   measured while the starting current flows from the U-phase to the V-phase. For the application of the starting current in accordance with another starting current pattern, it is also possible to measure the electromotive voltage of

15   one coil to which the current is not applied, among the U-phase coil 4a, the V-phase coil 4b and the W-phase coil 4c. The measurement of the electromotive voltage during the application of the starting current reduces the time required

20   for starting the brushless DC motor.

In succession, the drive operator 6 judges whether or not the electromotive voltage is induced in the armature 4 (Step S04). If the rotor 5 does not rotate, no electromotive voltage

25   is induced in the armature 4. A different operation is carried out depending on whether or not the electromotive voltage is induced in the

armature 4.

If the electromotive voltage is not induced in the armature 4, the drive operator 6 can not specify the position of the rotor 5. In this case, 5 the starting current pattern is switched to another pattern (Step S05). Moreover, the starting current is applied to the armature 4 in accordance with the switched starting current pattern (Step S02). The operation for switching 10 the starting current pattern is done until the slight rotation of the rotor 5 induces the electromotive voltage in the armature 4.

If the electromotive voltage is induced in the armature 4, the drive operator 6 judges the 15 rotation direction of the rotor 5 on the basis of the back electromotive voltage (Step S06).

If the drive operator 6 judges that the rotor 5 is rotated in an opposite direction of a desired direction, the drive operator 6 fails to 20 supply drive currents to the armature 4 to stop rotation of the rotor 5 (Step S07). In this case, the operations from the application of the starting current pattern (Step S02) to the judgement of the rotation direction of the rotor 25 5 (Step S06) are executed once again.

If the drive operator 6 judges that the rotor 5 is rotated in the desired direction, the

drive operator 6 carries out a closed loop drive

(Step S08). The drive operator 6 detects the

position of the rotor 5 on the basis of the

electromotive voltage induced in the armature 4.

5   Then the drive operator 6 determines the drive

current to be supplied to the U-phase coil 4a,

the V-phase coil 4b and the W-phase coil 4c on

the basis of the detected position. In succession

the drive operator 6 supplies the determined

10   drive current to drive the rotor 5. Once the

rotation of the rotor 5 is started, the position

of the rotor 5 is then detected on the basis of

the electromotive voltages induced in the

armature 4, and the rotor 5 is driven in response

15   to the detected position of the rotor 5.

At this time, the closed loop drive is done

while the duty of the drive current is set to

substantially 100 %. Here, when the drive current

is supplied only for τ (seconds) between two

20   phases among the U-phase, the V-phase and the W-

phase in a certain period having a length of T_1

(seconds), a duty D is defined as follows:

$$D = \tau / T_1$$

The fact that the duty is 100 % implies that the

25   drive current is continuously supplied between

the two phases among the U-phase, the V-phase and

the W-phase at any time. Fig. 7 shows the

potentials of the U-phase line 9a, the V-phase
line 9b and the W-phase line 9c when the duty is
100 %. With reference to Fig. 7, from a time t_1
to a time t_2, the W-phase line 9c is set at the

5 power supply potential V_{cc}, and the U-phase line
9a is set at the ground level. That is, from the
time t_1 to the time t_2, the drive current is
supplied from the W-phase of the armature 4 to
the U-phase. From the time t_2 to a time t_3, the

10 V-phase line 9b is set at the power supply
potential V_{cc}, and the U-phase line 9a is set at
the ground level. That is, from the time t_2 to
the time t_3, the drive current is supplied from
the V-phase of the armature 4 to the U-phase. In

15 this way, when the duty is 100 %, one line among
the U-phase line 9a, the V-phase line 9b and the
W-phase line 9c is set at the power supply
potential V_{cc} at any time, and another one line is
further set at the ground level. Thus, the drive

20 current is supplied between the two phases among
the U-phase, the V-phase and the W-phase. While
the closed loop drive is done with the duty
substantially 100 %, a possibly maximum torque
can be applied to the rotor 5.

25   In succession, the drive operator 6 judges
whether or not the rotor 5 is rotated (Step S09).
As mentioned above, since the starting current is

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applied to the armature 4 in accordance with the
determined starting current pattern, the rotor 5
is usually slightly rotated. However, if the
torque applied to the rotor 5 is weak at this
5 time, the start of the above-mentioned closed
loop drive (Step S08) may result in the stop of
the rotation of the rotor 5. Therefore, the drive
operator 6 judges whether or not the rotor 5 is
rotated on the basis of the electromotive voltage
10 induced in the armature 4.

If the rotor 5 is not rotated, the starting
current pattern is switched to another starting
current pattern (Step S10). Moreover, the
operations from the application of the starting
15 current pattern (Step S02) to the closed loop
drive at which the duty is 100 % (Step S08) are
executed once again.

If the rotor 5 is rotated, the closed loop
drive at which the duty is 100 % is continued
20 (Step S11). The closed loop drive at which the
duty is 100 % is continued until the speed of
rotation of the rotor 5 reaches the predetermined
speed of rotation (Step S12).

After the speed of rotation of the rotor 5
25 reaches the predetermined speed of rotation, the
closed loop drive is executed while the duty is
controlled on the basis of the speed of rotation

of the rotor 5 (Step S13). The control of the duty enables the desirable torque to be applied to the rotor 5 to control the rotation speed of the rotor5. The starting of the brushless DC

5 motor is completed by the above-mentioned processes.

In the above-mentioned method of actuating a brushless DC motor, The judgment of the rotation direction in Step S06 may be canceled

10 (Step S06). Also in this case, the rotor 5 is rotated in the desired rotation direction, since the closed loop drive is done on the basis of the detected position of the rotor 5. However, if the judgment of the rotation direction (Step S06) is

15 not done, the rotor 5 may be reversed to rotate in the desired direction when the stating current rotates the rotor 5 in the opposite direction of the desired direction. Thus, it is desirable that the judgment of the rotation direction (Step S06)

20 is done.

The brushless DC motor in this embodiment and the method of starting the same need not wait for the situation that the rotor 5 is locked at a certain position. The brushless DC motor and

25 method of starting the same reduces the time necessary for the actuation.

Also, in the brushless DC motor and the

method of starting the same, it is not necessary to use the memory having the large circuit size. Moreover, the brushless DC motor and the method of starting the same, it is not necessary to

5   mount the analog circuit.   In the brushless DC motor and the method of actuating the same, it is possible to reduce the circuit sizes of the induced voltage detector 2 and the driver 3. Moreover, in the brushless DC motor and the

10   method of actuating the same, if the induced voltage detector 2 and the driver 3 are integrated into LSI, it is possible to reduce the occupation area.

Although the invention has been described

15   in its preferred form with a certain degree of particularity, it is understood that the present disclosure of the preferred form has been changed in the details of construction and the combination and arrangement of parts may be

20   resorted to without departing from the spirit and the scope of the invention as hereinafter claimed.